

FORM PTO-1390 REV. 5-93		US DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE	ATTORNEYS DOCKET NUMBER P00,1899
TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371			U.S. APPLICATION NO. (if known, see 37 CFR 1.5) 09/720999
INTERNATIONAL APPLICATION NO. PCT/DE99/01700	INTERNATIONAL FILING DATE 10 June 1999	PRIORITY DATE CLAIMED 08 July 1998	
TITLE OF INVENTION ENGRAVING ELEMENT			
APPLICANT(S) FOR DO/EO/US Dieter Carstens			
Applicant herewith submits to the United States /Designated/Elected Office (DO/EO/US) the following items and other information:			
<ol style="list-style-type: none"> 1. <input checked="" type="checkbox"/> This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 2. <input type="checkbox"/> This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 3. <input checked="" type="checkbox"/> This express request to begin national examination procedures (35 U.S.C. 371(f)) at any time rather than delay. 4. <input checked="" type="checkbox"/> A proper Demand for International Preliminary Examination will be made by the 19th month from the earliest claimed priority date. 5. <input checked="" type="checkbox"/> A copy of International Application as filed (35 U.S.C. 371(c)(2)) <ol style="list-style-type: none"> a. <input checked="" type="checkbox"/> is transmitted herewith (required only if not transmitted by the International Bureau). b. <input type="checkbox"/> has been transmitted by the International Bureau. c. <input type="checkbox"/> is not required, as the application was filed in the United States Receiving Office (RO/US) 6. <input checked="" type="checkbox"/> A translation of the International Application into English (35 U.S.C. 371(c)(2)). 7. <input checked="" type="checkbox"/> Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. §371(c)(3)) <ol style="list-style-type: none"> a. <input type="checkbox"/> are transmitted herewith (required only if not transmitted by the International Bureau). b. <input type="checkbox"/> have been transmitted by the International Bureau. c. <input type="checkbox"/> have not been made; however, the time limit for making such amendments has NOT expired. d. <input checked="" type="checkbox"/> have not been made and will not be made. 8. <input type="checkbox"/> A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)). 9. <input checked="" type="checkbox"/> An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)). Unexecuted 10. <input checked="" type="checkbox"/> A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)). 			
Items 11. to 16. below concern other document(s) or information included:			
11. <input checked="" type="checkbox"/> An Information Disclosure Statement under 37 C.F.R. 1.97 and 1.98; (PTO 1449, Prior Art, Search Report).			
12. <input type="checkbox"/> An assignment document for recording A separate cover sheet in compliance with 37 C.F.R. 3.28 and 3.31 is included. (SEE ATTACHED ENVELOPE)			
13. <input type="checkbox"/> A FIRST preliminary amendment. <input type="checkbox"/> A SECOND or SUBSEQUENT preliminary amendment.			
14. <input checked="" type="checkbox"/> A substitute specification. - Marked up copy			
15. <input type="checkbox"/> A change of power of attorney and/or address letter.			
16. <input checked="" type="checkbox"/> Other items or information: <ol style="list-style-type: none"> a. <input checked="" type="checkbox"/> Submission of Drawings - Eight sheets of Drawings - b. <input checked="" type="checkbox"/> EXPRESS MAIL #EL655302815US dated January 3, 2001. 			

09/720999

PCT/DE99/01700

BASIC NATIONAL FEE (37 C.F.R. 1.492(a)(1)-(5):

- ☒ Search Report has been prepared by the EPO or JPO \$860.00
- International preliminary examination fee paid to USPTO (37 C.F.R. 1.482) \$690.00
- No international preliminary examination fee paid to USPTO (37 C.F.R. 1.482) but international search fee paid to USPTO (37 C.F.R. 1.445(a)(2)) \$760.00
- Neither international preliminary examination fee (37 C.F.R. 1.482) nor international search fee (37 C.F.R. 1.445(a)(2)) paid to USPTO \$970.00
- International preliminary examination fee paid to USPTO (37 C.F.R. 1.482) and all claims satisfied provisions of PCT Article 33(2)-(4) \$96.00

ENTER APPROPRIATE BASIC FEE AMOUNT =

\$860.00

Surcharge of \$130.00 for furnishing the oath or declaration later than ☐ 20 ☐ 30 months from the earliest claimed priority date (37 C.F.R. 1.492(e)).

\$ 0

Claims

Number Filed

Number
Extra

Rate

Total Claims

14

- 20 =

0

X \$ 18.00

\$ 0

Independent Claims

4

- 3 =

1

X \$ 80.00

\$ 80.00

Multiple Dependent Claims

\$270.00 +

\$

TOTAL OF ABOVE CALCULATIONS =

\$940.00

Reduction by 1/2 for filing by small entity, if applicable. Verified Small Entity statement must also be filed. (Note 37 C.F.R. 1.9, 1.27, 1.28)

\$

SUBTOTAL =

\$940.00

Processing fee of \$130.00 for furnishing the English translation later than ☐ 20 ☐ 30 months from the earliest claimed priority date (37 CFR 1.492(f)).

\$

+

TOTAL NATIONAL FEE =

\$940.00

Fee for recording the enclosed assignment (37 C.F.R. 1.21(h). The assignment must be accompanied by an appropriate cover sheet (37 C.F.R. 3.28, 3.31). \$40.00 per property

+

TOTAL FEES ENCLOSED =

\$940.00

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- a. ☒ A check in the amount of \$ **940.00** to cover the above fees is enclosed.
- b. ☐ Please charge my Deposit Account No. _____ in the amount of \$ _____ to cover the above fees. A duplicate copy of this sheet is enclosed.
- c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. **501519**. A duplicate copy of this sheet is enclosed.

NOTE: Where an appropriate time limit under 37 C.F.R. 1.494 or 1.495 has not been met, a petition to revive (37 C.F.R. 1.137(a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO:

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Registration Number

09/720999

525 Rec'd PCT/PTO 03 JAN 2001

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BOX PCT
IN THE UNITED STATES ELECTED OFFICE
OF THE UNITED STATES PATENT AND TRADEMARK OFFICE
UNDER THE PATENT COOPERATION TREATY-CHAPTER II

5

PRELIMINARY AMENDMENT

APPLICANTS: DIETER CARSTENS

DOCKET NO: P00,1899

SERIAL NO:

GROUP ART UNIT:

EXAMINER:

10 INTERNATIONAL APPLICATION NO: PCT/DE99/01700

INTERNATIONAL FILING DATE: 10 June 1999

INVENTION: "ENGRAVING ELEMENT"

Assistant Commissioner for Patents,
Washington, D.C. 20231

15 Sir:

As a Preliminary Amendment for entry into the
National Stage for the above-identified PCT application,
the following is submitted:

IN THE ABSTRACT:

20 Please cancel the previous Abstract and substitute
the new Abstract attached herewith on a separate sheet
as part of the Substitute Specification.

IN THE SPECIFICATION:

25 Please enter the enclosed Substitute Specification
in place of the PCT translation together with the PCT

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substitute pages 3 and 3a entered in the PCT Chapter II prosecution. There is no new matter in the Substitute Specification. A marked up copy of the specification showing the changes in the Substitute Specification is enclosed.

IN THE CLAIMS:

On page 11 of the claims, delete "Patent Claims" and substitute --I CLAIM AS MY INVENTION--.

Please cancel claims 1-10 entered as substitute pages (annexes) in the PCT prosecution and substitute new claims 11-24 as follows:

11. An engraving element of an electronic engraving machine for engraving printing forms, comprising:

a shaft oscillating around a longitudinal axis with small rotational angles;

a drive system for the shaft;

a lever attached to an end of the shaft with an engraving stylus for engraving the printing form;

a restoring element for the shaft;

a damping mechanism for the shaft having a damping element secured to the shaft as well as a stationary damping chamber filled with a damping medium connected to the shaft via a bearing;

the damping element being formed of at least one damping disk that is circular at least in regions and extending perpendicular to the shaft;

the damping chamber being designed at least as a hollow-cylindrical segment around the shaft into which the damping disk projects;

the damping chamber extending at least over the
circular regions of the damping disk; and
the damping medium being a ferro-fluidic fluid.

12. The engraving element according to claim
5 11 wherein the damping mechanism is not rotationally
symmetrical relative to an axial direction of the shaft.

13. The engraving element according to claim
11 wherein the damping element is provided with through
holes proceeding in an axial direction of the shaft.

10 14. The engraving element according to claim
11 wherein the bearing connected to the shaft comprises
a spoke bearing.

15 15. The engraving element according to claim
14 wherein the spoke bearing is formed of:

an inner ring surrounding and connected to the
shaft;

one of a stationary outer ring and an outer ring
segment surrounding the shaft at least in regions and
spaced from the inner ring; and

20 a plurality of leaf springs proceeding radially
relative to the shaft whose ends are respectively
connected to the inner ring and to one of the outer ring
and the outer ring segment.

16. the engraving element according to claim 14 wherein the damping mechanism and the spoke bearing are structurally united with one another.

5 17. The engraving element according to claim 11 wherein the drive system for the shaft is designed as one of a piezoelectric and a magnetostrictive drive element.

18. The engraving element according to claim 11 wherein the bearing has a flexible member.

10 19. A damping mechanism for an engraving element for engraving printing forms, comprising:

a damping element secured to a shaft of the engraving element oscillating around a longitudinal axis with small rotational angles;

15 a stationary damping chamber filled with a damping medium;

the damping element being formed of at least one damping disk circular at least in regions and extending perpendicular to the shaft;

20 the damping chamber being designed at least as a hollow-cylindrical segment around the shaft into which the damping disk projects;

the hollow-cylindrical damping chamber extending at least over the circular regions of the damping disk; and

25 the damping medium comprising a ferro-fluidic fluid.

20. The damping mechanism according to claim 19 wherein it has a shape which is not rotational-symmetrical to an axial direction of the shaft.

21. The damping mechanism according to claim 5 19 wherein the damping element is provided with through holes proceeding in an axial direction of the shaft.

22. The damping mechanism according to claim 19 wherein the stationary damping chamber is connected to the shaft by a flexible bearing.

10 23. The damping mechanism of claim 22 wherein the flexible bearing has leaf spring spokes.

24. A damping mechanism for an engraving element for engraving printing forms, comprising:

15 a damping element secured to a shaft of the engraving element oscillating around a longitudinal axis;

a damping chamber filled with a damping medium;

the damping element being formed of at least one damping disk and extending perpendicular to the shaft;

20 the damping chamber being designed at least as a hollow-cylindrical segment around the shaft into which the damping disk projects;

the hollow-cylindrical damping chamber extending over the damping disk; and

25 the damping medium comprising a ferro-fluidic fluid.


REMARKS

The specification, and abstract have been amended in accordance with U. S. practice and for improved readability and clarity.

5 New claims drawn in accordance with U. S. practice are presented. These claims generally relate to the claims prosecuted (that is the substitute page claims 1-10) in the PCT prosecution.

An Information Disclosure Statement is enclosed.

10 Respectfully submitted,

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SPECIFICATION

TITLE

ENGRAVING ELEMENT

5

BACKGROUND OF THE INVENTION

The invention is in the field of electronic reproduction technology and is directed to an engraving element for engraving printing forms for rotogravure as well as to a damping mechanism for an engraving element.

10

In an electronic engraving machine, an engraving element with an engraving stylus as a cutting tool moves along a rotating printing cylinder in the axial direction. The engraving stylus controlled by an engraving control signal cuts a sequence of cups arranged in a rotogravure raster into the generated surface of the printing cylinder. The engraving control signal is formed by superimposition of a

15 periodic raster signal with image signal values that represent the hues to be reproduced between "black" and "white". Whereas the raster signal effects a vibrating lifting motion of the engraving stylus for generating the rotogravure raster, the image signal values control the cutting depths of the engraved cups in conformity with the hues to be reproduced.

20

DE-A-23 36 089 discloses an engraving element with an electromagnetic drive element for the engraving stylus. The electromagnetic drive element is composed of a stationary electromagnet charged with the engraving control signal in whose air gap the armature of a rotatory system moves. The rotatory system is composed of a shaft, the armature, a bearing for the shaft and of a damping

25 mechanism. One shaft end merges into a stationarily clamped resilient torsion rod, whereas the other shaft end carries a lever to which the engraving stylus is attached. An electrical torque is exerted on the armature of the shaft by the magnetic field generated in the electromagnet, this electrical torque being opposed by the mechanical torque of the torsion rod. The electrical torque turns the shaft around its longitudinal

30 axis by a rotational angle proportional to the respective image signal value, turning

Substitute specification

this from a quiescent position, and the torsion rod guides the shaft back into the quiescent position.

Due to the rotational movement of the shaft around the longitudinal axis, the engraving stylus executes a lifting motion directed in the direction onto the generated surface of the printing cylinder, this respectively defining the penetration depth of the engraving stylus into the printing cylinder.

The damping mechanism serves the purpose of defined damping of rotational oscillations and transverse oscillations of the rotatory system and, thus, for damping the movement of the engraving stylus.

Given, in particular, sudden changes in the image signal values at steep density transitions (contours), the engraving stylus can exhibit a faulty activation and deactivation behavior that is essentially dependent on the degree of damping achieved in the damping mechanism. The consequence of a faulty activation behavior of the engraving stylus is engraving errors on the printing cylinder or disturbing changes in hue in the print.

Given inadequate damping of the rotatory system, disturbing multiple contours arise at density discontinuities due to over-shooting of the engraving stylus. Given too great a damping of the rotatory system, the engraving stylus cannot follow fast enough at steep density transitions, and the rated engraving depth is only achieved or left at a distance following the density discontinuity, as a result whereof steep density discontinuities are reproduced in unsharp fashion.

Moreover, a high temperature and long-term stability of the degree of attenuation are required.

The quality in the engraving of printing forms is thus influenced substantially by the degree of damping of the engraving element.

In a first exemplary embodiment, the damping mechanism disclosed by DE-A-23 36 089 is composed of a damping element connected to the shaft of the engraving element that immerses into a stationary damping chamber filled with a

damping grease as damping agent. The damping element is designed as a circular damping disk or has at least one damping wing. A damping grease loses its damping properties over time due to the mechanical stressing and thus does not exhibit the required long-term stability.

5 In a second exemplary embodiment, the damping mechanism disclosed by DE-A-23 36 089 comprises two or more identical damping elements axially symmetrically at the circumference and stationarily connected at the outside to a seat, these damping elements residing under pre-stress in the radial direction. The damping elements are composed of an elastic-plastic synthetic, for example of a fluor-
10 elastomer. The degree of attenuation that can be achieved at the moment with an elastic-plastic synthetic is dependent on the respectively preceding shaping. This "memory" effect disadvantageously leads to the fact that the engraving stylus achieves and in turn departs the rated engraving depth only with a disturbing delay.

15 In order to achieve a higher engraving speed, efforts have been undertaken to increase the engraving frequency, i.e. the frequency of the raster signal. A higher engraving frequency, however, leads to an increased production of heat in the engraving element. The employment of damping elements composed of an elastic-plastic synthetic has the further disadvantage that this does not eliminate the heat fast enough, this potentially leading to a modification for the degree of damping and, thus,
20 to disturbing engraving errors.

US-4,357,633 recites another electro-mechanical engraving element having a damping mechanism. The damping mechanism is composed of a circular damping disk connected to the shaft and of a stationary, annular bearing disk between which damping elements composed of an elastic, non-compressible material are
25 arranged.

US-4,123,675 discloses a damping mechanism for a stepping motor drive, whereby a magnetic disk with high inertia floats in a housing filled with a ferro-fluid. The housing is rigidly connected to the shaft of the stepping motor, i.e. it turns

together with the stepping motor, and the friction between the inside housing wall and the inertial disk effects the damping.

SUMMARY OF THE INVENTION

5 The invention is based on the object of improving an engraving element of an electronic engraving machine for engraving printing forms as well as a damping mechanism for an engraving element such that the movement of the engraving stylus of the engraving element is optimally damped in order to achieve a high engraving quality.

10 According to the invention, an engraving element of an electronic engraving machine for engraving printing forms has a shaft oscillating around a longitudinal axis with small rotational angles. A drive system is provided for the shaft. A lever attaches to an end of the shaft with an engraving stylus for engraving the printing form. A restoring element is provided for the shaft. An adapting
15 mechanism for the shaft has a damping element secured to the shaft as well as a stationary damping chamber filled with a damping medium connected to the shaft via a bearing. The damping element is formed of at least one damping disk that is circular at least in regions and extending perpendicular to the shaft. The damping chamber is designed at least as a hollow cylindrical segment around the shaft into
20 which the damping disk projects. The damping chamber extends at least over the circular regions of the damping disk. The damping medium is a ferro-fluidic fluid.

 The invention is explained in greater detail below with reference to Figs. 1
5 through 9.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic structure of an engraving element having a damping mechanism in a perspective view;

5 Fig. 2 is an exemplary embodiment of a rotational-symmetrical damping mechanism having a circular or circular sector-shaped damping disk, shown in section;

Fig. 3 is an exemplary embodiment of a non-rotational symmetrical damping mechanism having a circular segment-shaped damping disk, shown in section;

10 Fig. 4 is an exemplary embodiment of a rotational-symmetrical damping mechanism having two circular or circular sector-shaped damping disks, shown in section;

15 Fig. 5 is an exemplary embodiment of a non-rotational-symmetrical damping mechanism having two circular segment-shaped damping disks, shown in section;

Fig. 6 is a development of a rotational-symmetrical damping mechanism having an integrated spoke bearing, shown in section;

Fig. 7 is a development of a non-rotational-symmetrical damping mechanism having an integrated spoke bearing, shown in section;

20 Fig. 8 is a perspective illustration of a rotationally symmetrically designed spoke bearing; and

Fig. 9 is a perspective illustration of a non-rotationally symmetrically designed spoke bearing.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

25 Fig. 1 shows a perspective illustration of the structure of an engraving element that is fundamentally composed of a drive system - of an electromagnetic drive system in the illustrated example - and of a rotatory system.

Substitute specification

The electromagnetic drive element is composed of a stationary
 electromagnet 1 having two u-shaped plate packets 2 lying opposite one another and
 two air gaps 3 lying between the legs of the plate packets 2. A coil 5 - which is shown
 from only the coil side - is located in the recesses 4 of the plate packets 2 of the
 5 electromagnet 1. The coil 5 has an engraving control signal flowing through it.

The rotatory system is composed of a shaft 6, of an armature 7 secured to
 the shaft 6, as well as of a damping mechanism 8 and a spoke bearing 9 for the shaft
 6. The armature 7 is movable in the air gaps 3 of the electromagnet 1. One shaft end
 merges into a resilient torsion bar 10 that is clamped in a stationary bearing 11, 12.
 10 The other shaft end 13 carries a lever 14 to which the engraving stylus 15 is attached.
 The damping mechanism 8 and the spoke bearing 9 are arranged between the armature
 7 and the lever 14 with the engraving stylus 15. As a result of the magnetic field
 generated in the air gaps 3 of the electromagnet 1, an electrical torque is exerted on
 the armature 7 of the shaft 6, this electrical torque being opposed by the mechanical
 15 torque of the torsion bar 10. The electrical torque turns the shaft 6 around its
 longitudinal axis with a rotational angle proportional to the respective engraving
 control signal value, turning this out of a quiescent position, and the torsion bar 10
 returns the shaft 6 into the quiescent position. As a result of the rotatory motion of the
 shaft 6, the engraving stylus 15 implements a stroke directed in the direction onto the
 20 generated surface of a printing cylinder (not shown) that defines the penetration depth
 of the engraving stylus 15 into the printing cylinder. When engraving, the rotatory
 system executes an oscillation motion dependent on the frequency of the raster signal
 by a very small rotational angle of, for example, a maximum of $\pm 0.5^\circ$, this
 corresponding to a maximum stroke of approximately 250 μm of the engraving stylus
 25 15.

The drive system for the engraving stylus 15 can also be designed as a
 solid-state actuator element that, for example, can be formed of a piezoelectric or of a
 magnetostrictive material.

Substitute specification

Figs. 2a, 2b show an exemplary embodiment of a rotational-symmetrical damping mechanism 8 having a circular or circular sector-shaped damping disk 17.

Fig. 2a shows a sectional view of the damping mechanism 8 in an axial direction of the shaft 6. The damping mechanism 8 is essentially composed of a damping disk 17 that is connected to the shaft 6 and expands perpendicular to the shaft 6 and is further composed of a stationary damping chamber 18. The damping disk 17 is designed as at least one damping wing (Fig. 2c) rotational-symmetrically relative to the shaft 6 either circularly (Fig. 2b) or circular sector-shaped. The stationary damping chamber 18 is designed as a rotational-symmetrical hollow cylinder around the shaft 6 having a u-shaped cross-section into whose interior facing toward the shaft 6 the damping disk 17 immerses. When the damping disk 17 is designed as at least one damping wing, the damping chamber 18 can be composed of hollow cylinder segments that respectively extend at least over a damping wing 17. The stationary damping chamber 18 is composed of a disk-shaped base plate 20, of a disk-shaped cover plate 21 and of a spacer ring 22 lying between base plate 20 and cover plate 21. The base plate 20 and the cover plate 21 comprise through openings 23, 24 for the shaft 6. Base plate 20, cover plate 21 and spacer ring 22 are arranged such relative to one another and connected to one another with, for example, screws 25 such that they form the interior of the damping chamber 18. The spacer ring 22 is dimensioned such that a defined damping gap 26 for the acceptance of a damping fluid arises between base plate 20, cover plate 21 and spacer ring 22 on the one hand and the damping surfaces of the damping disk 17 on the other hand.

The diameter of the through opening 24 in the cover plate 21 is selected such that an additional damping gap 26' for the damping fluid is formed between the inside surface that faces toward the shaft 6 and the generated surface of the shaft 6. The damping disk 17 can be provided with through holes 27 proceeding in the axial direction of the shaft 6. The through holes 27 form connecting channels to the damping gaps 26 above and below the damping disk 17 and advantageously serve for

Substitute specification

compensating the damping fluid and as a reservoir for the damping fluid. Over and above this, the through holes 27 reduce axial vibrations of the damping disk 17.

A ferro-fluidic fluid is preferably employed as a damping fluid in the damping chamber (18). A ferro-fluidic fluid is a colloidal solution of magnetic particles in an oil that can be magnetized. A ferro-fluidic fluid is commercially obtainable under the trade name Ferrofluidics® of ferro fluidics GmbH.

The degree of attenuation that can be achieved with a damping fluid is advantageously independent of the respectively preceding deformation, so that no "memory" effect arises that would lead to disturbing engraving errors. Over and above this, the degree of damping that can be achieved with a damping fluid can be approximately calculated. A high temperature stability and long-term stability of the degree of damping is also achieved with a damping fluid, since the heat arising as a result of high engraving frequencies can be eliminated well via the damping fluid. The described exemplary embodiment employs a ferrofluidic damping fluid that is held in the damping gap 26 by a magnetic field generated with a magnet, as a result whereof complicated seals can be eliminated. In the exemplary embodiment, an annular retaining magnet 28 for the ferro-fluid is located in an annular channel 29 in the base plate 20 of the damping chamber 18. In order to prevent dust from entering into the damping chamber 18, a seal ring 30 embracing the shaft 6 can be provided, this being located in a recess 31 of the base plate 20.

Fig. 2b shows a section through the damping mechanism 8 in a plane proceeding perpendicular to the axial direction of the shaft 6. The sectional view shows the circularly designed damping disk 17.

Fig. 2c again shows a section through the damping mechanism 8 in a plane proceeding perpendicular to the axial direction of the shaft 6. The sectional view shows the design of the circular sector-shaped damping disk 17 as two damping wings.

Fig. 3 shows an exemplary embodiment of a non-rotational-symmetrical damping mechanism 8 having a circular segment-shaped damping disk 1.

Fig. 3a again shows a section through the damping mechanism 8 in the axial direction of the shaft 6, whereby the damping disk 17 and the damping chamber 18 are designed as circular or hollow-cylindrical segments that are not rotationally symmetrical with respect to the axis of the shaft 6. This embodiment can be advantageously employed when an optimally slight distance of the shaft 6 of the engraving element from the generated surface of a printing cylinder is desired. The damping disk 17 is designed as a circular segment, whereby the edge of the damping disk 17 forming the chord lies as close as possible to the shaft 6. The damping chamber 18 is designed as a hollow cylinder segment corresponding to the shape of the damping disk 17 designed as a circular segment. The fundamental structure of the damping chamber 18 is basically identical to the structure of the damping chamber 18 shown in Fig. 2a.

Fig. 3b shows a section through the damping mechanism 8 in a plane proceeding perpendicular to the axial direction of the shaft 6. The sectional view shows the design of the damping disk 17 as circular segment.

Fig. 4 shows an exemplary embodiment of a rotational-symmetrical damping mechanism 8 having two circular or circular sector-shaped damping disks 17, 17' in a section in an axial direction of the shaft 6.

The damping mechanism 8 is basically constructed like the damping mechanism 8 according to Fig. 2a. It differs from the damping mechanism (8) shown in Fig. 2a in that two damping disks 17, 17' arranged parallel to one another and spaced from one another in the axial direction of the shaft 6 are connected as a double disk to the shaft 6, and in that the damping chamber 18 is divided by an intermediate plate 32 in two sub-chambers 33, 33' for the two damping disks 17, 17'. The intermediate plate 32 is thereby dimensioned such that the two sub-chambers 33, 33'

are connected to one another by an additional damping gap 26'. The damping disks (17, 17') are shaped as shown in Fig. 2a or Fig. 2c).

Fig. 5 shows an exemplary embodiment of a non-rotational-symmetrical damping mechanism 8 having two circular segment-shaped damping disks 17, 17' in a sectional view in the axial direction of the shaft 6. The damping mechanism 8 is fundamentally constructed as described in Fig. 4. The damping disks 17, 17' are shaped as shown in Fig. 3b.

The damping disk 17 is made, for example, of aluminum or steel. Base plate 20, cover plate 21, spacer ring 22 and intermediate plate 32 are preferably composed of non-magnetic material.

The two damping disks 17, 17' can be supplemented by further damping disks. The employment of more than one damping disk has the advantage that a higher degree of damping is achieved due to the increased damping area that interacts with the damping fluid. Given an identical damping area, the diameter of the individual damping disks can be reduced given employment of a plurality of damping disks. This preferably leads to a lower mass moment of inertia and to lower circumferential speeds at the edges of the damping disks. This reduces the risk that the damping fluid will modify and deteriorate the damping property.

Fig. 6 shows a development wherein the rotational-symmetrical damping mechanism 8 is structurally combined with the rotational-symmetrically fashioned spoke bearing 9.

Fig. 6a shows a section through the damping mechanism 8 in the axial direction of the shaft 6, this agreeing with the sectional view of the damping mechanism 8 shown in Fig. 2a except for the spoke bearing 9. The rotational-symmetrical spoke bearing 9 is composed of an inside ring 35 embracing the shaft 6 and connected thereto, of a stationary outer ring 36 surrounding the shaft 6 and spaced from the inner ring 35, and of a plurality of leaf springs 37 proceeding radially at identical or irregular angular spacings. The broadsides are directed in the axial

direction of the shaft 6, so that the inner ring 35 is torsionally seated relative to the stationary outer ring 36, namely around the longitudinal axis of the shaft 6. The ends of the leaf springs 37 are respectively clamped in the two rings 35, 36. Outer ring 36 and cover plate 21 of the damping chamber 18 are preferably fabricated as one component part.

Fig. 6b shows a section through the rotational-symmetrical spoke bearing 9 in a plane proceeding perpendicular to the axial direction of the shaft 6.

Fig. 7 shows a development wherein the non-rotational-symmetrical damping mechanism 8 is structurally united with the non-rotationally-symmetrically designed spoke bearing 9.

Fig. 7a shows a section through the non-rotational-symmetrical damping mechanism 8 in the axial direction of the shaft 6, this coinciding with the section through the damping mechanism 8 shown in Fig. 3a except for the structurally integrated spoke bearing 9. The non-rotational-symmetrical spoke bearing 9 is composed of an inner ring 35 that surrounds the shaft 36 and is connected thereto, of a stationary outer ring segment 36' that surrounds the shaft 6 and is spaced from the inner ring 35', and of a plurality of radially proceeding leaf springs 37' whose broad sides are likewise directed in axial direction of the shaft 6 and whose ends are respectively secured in the inner ring 35' and in the outer ring segment 36'. Outer ring segment 36' and circular segment-shaped cover plate 21 of the damping chamber 18 are again a shared component part.

Fig. 7b shows a section through the non-rotational-symmetrical spoke bearing 9 in a plane proceeding perpendicular to the axial direction of the shaft 6.

Fig. 8 shows a perspective view of a rotational-symmetrically fashioned spoke bearing 9.

Fig. 9 shows a perspective view of a non-rotational-symmetrically designed spoke bearing 9.

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	

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ABSTRACT

An engraving element of an electronic engraving machine for engraving printing forms is formed of a shaft oscillating around a longitudinal axis with small rotational angles. A drive system is provided for the shaft with a lever attached to one end of the shaft. An engraving stylus is provided for engraving the printing form, along with a restoring element for the shaft, a bearing for the shaft, and a damping mechanism for the shaft having a damping element secured to the shaft and a stationary damping chamber. The damping element comprises at least one damping disk that is designed circularly at least in regions and extends perpendicular to the shaft. The damping chamber is designed at least as a hollow-cylindrical segment around the shaft into which the damping disk projects and extends at least over the circular region of the damping disk. The damping chamber is filled with a ferro-fluidic fluid as a damping agent.



PCT WELTORGANISATION FÜR GEISTIGES EIGENTUM
Internationales Büro
INTERNATIONALE ANMELDUNG VERÖFFENTLICHT NACH DEM VERTRAG ÜBER DIE
INTERNATIONALE ZUSAMMENARBEIT AUF DEM GEBIET DES PATENTWESENS (PCT)

(51) Internationale Patentklassifikation ⁷ :

B41C 1/04, H02K 37/22

A1

(11) Internationale Veröffentlichungsnummer: **WO 00/02728**

(43) Internationales
Veröffentlichungsdatum:

20. Januar 2000 (20.01.00)

(21) Internationales Aktenzeichen: PCT/DE99/01700

(22) Internationales Anmeldedatum: 10. Juni 1999 (10.06.99)

(30) Prioritätsdaten:

198 30 471.4

8. Juli 1998 (08.07.98)

DE

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(81) Bestimmungsstaaten: CN, JP, US, europäisches Patent (AT,
BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU,
MC, NL, PT, SE).

Veröffentlicht

Mit internationalem Recherchenbericht.

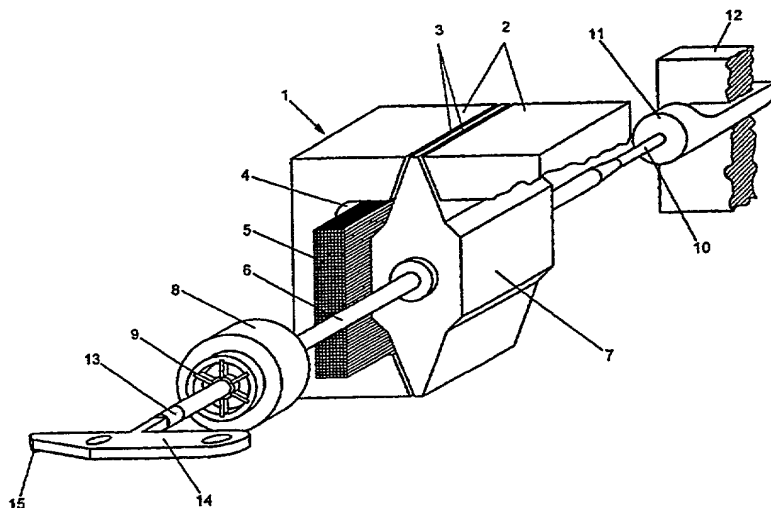
*Vor Ablauf der für Änderungen der Ansprüche zugelassenen
Frist; Veröffentlichung wird wiederholt falls Änderungen
eintreffen.*

(54) Title: ENGRAVING MEMBER

(54) Bezeichnung: GRAVIERORGAN

(57) Abstract

The invention relates to an engraving member pertaining to an electronic engraving machine used to engrave printing forms. The engraving member consists of a shaft (6) that oscillates around the longitudinal axis at low angles of rotation, a drive system (1,7) for said shaft (6), a lever (14) mounted on one end of the shaft (6) and provided with a burin (15) in order to engrave a printing form, a reset element (11) for the shaft (6), a bearing (98) for the shaft (6) and a damping device (8) for the shaft, consisting of a damping element secured to the shaft (6) and a fixed damping chamber. The damping element has at least one damping disk that is at least circular in certain areas and extends perpendicular to the shaft (6). The damping chamber is formed by at least one hollow cylindrical segment around the shaft (6). The damping disk protrudes into said hollow cylindrical segment and the damping chamber extends at least partially over the circular area of the damping disk. The damping chamber is filled with a ferrofluid that acts as a damping agent.



ENGRAVING ELEMENT

The invention is in the field of electronic reproduction technology and is directed to an engraving element for engraving printing forms for rotogravure as well as to a damping mechanism for an engraving element.

5 In an electronic engraving machine, an engraving element with an engraving stylus as cutting tool moves along a rotating printing cylinder in axial direction. The engraving stylus controlled by an engraving control signal cuts a sequence of cups arranged in a rotogravure raster into the generated surface of the printing cylinder. The engraving control signal is formed by superimposition of a
10 periodic raster signal with image signal values that represent the hues to be reproduced between "black" and "white". Whereas the raster signal effects a vibrating lifting motion of the engraving stylus for generating the rotogravure raster, the image signal values control the cutting depths of the engraved cups in conformity with the hues to be reproduced.

15 DE-A-23 36 089 discloses an engraving element with an electromagnetic drive element for the engraving stylus. The electromagnetic drive element is composed of a stationary electromagnet charged with the engraving control signal in whose air gap the armature of a rotatory system moves. The rotatory system is composed of a shaft, the armature, a bearing for the shaft and of a damping
20 mechanism. One shaft end merges into a stationarily clamp, resilient torsion rod, whereas the other shaft end carries a lever to which the engraving stylus is attached. An electrical torque is exerted on the armature of the shaft by the magnetic field generated in the electromagnet, this electrical torque being opposed by the mechanical torque of the torsion rod. The electrical torque turns the shaft around its longitudinal
25 axis by a rotational angle proportional to the respective image signal value, turning this from a quiescent position, and the torsion rod guides the shaft back into the quiescent position.

Due to the rotational movement of the shaft around the longitudinal axis, the engraving stylus executes a lifting motion directed in the direction onto the

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generated surface of the printing cylinder, this respectively defining the penetration depth of the engraving stylus into the printing cylinder.

The damping mechanism serves the purpose of defined damping of rotational oscillations and transverse oscillations of the rotatory system and, thus, for
5 damping the movement of the engraving stylus.

Given, in particular, sudden changes in the image signal values at steep density transitions (contours), the engraving stylus can exhibit a faulty activation and deactivation behavior that is essentially dependent on the degree of damping achieved in the damping mechanism. The consequence of a faulty activation behavior of the
10 engraving stylus is engraving errors on the printing cylinder or, respectively, disturbing changes in hue in the print.

Given inadequate damping of the rotatory system, disturbing multiple contours arise at density discontinuities due to over-shooting of the engraving stylus. Given too great a damping of the rotatory system, the engraving stylus cannot follow
15 fast enough at steep density transitions, and the rated engraving depth is only achieved or left at a distance following the density discontinuity, as a result whereof steep density discontinuities are reproduced unsharp.

Moreover, a high temperature and long-term stability of the degree of attenuation are required.

20 The quality in the engraving of printing forms is thus influenced substantially by the degree of damping of the engraving element.

In a first exemplary embodiment, the damping mechanism disclosed by DE-A-23 36 089 is composed of a damping element connected to the shaft of the engraving element that immerses into a stationary damping chamber filled with a
25 damping grease as damping agent. The damping element is fashioned as a circular damping disk or has at least one damping wing. A damping grease loses its damping properties over time due to the mechanical stressing and thus does not exhibit the required long-term stability.

In a second exemplary embodiment, the damping mechanism disclosed by
30 DE-A-23 36 089 comprises two or more identical damping elements axially symmetrically at the circumference and stationarily connected at the outside to a seat,

these damping elements residing under pre-stress in radial direction. The damping elements are composed of an elastic-plastic synthetic, for example of a fluor-elastomer. The degree of attenuation that can be achieved at the moment with an elastic-plastic synthetic is dependent on the respectively preceding shaping. This
5 "memory" effect disadvantageously leads to the fact that the engraving stylus achieves and in turn departs the rated engraving depth only with a disturbing delay.

In order to achieve a higher engraving speed, efforts have been undertaken to increase the engraving frequency, i.e. the frequency of the raster signal. A higher engraving frequency, however, leads to an increased production of heat in the
10 engraving element. The employment of damping elements composed of an elastic-plastic synthetic has the further disadvantage that this does not eliminate the heat fast enough, this potentially leading to a modification for the degree of damping and, thus, to disturbing engraving errors.

US-4,357,633 recites another electro-mechanical engraving element
15 having a damping mechanism. The damping mechanism is composed of a circular damping disk connected to the shaft and of a stationary, annular bearing disk between which damping elements composed of an elastic, non-compressible material are arranged.

US-4,123,675 discloses a damping mechanism for a stepping motor drive,
20 whereby a magnetic disk with high inertia floats in a housing filled with a ferro-fluid. The housing is rigidly connected to the shaft of the stepping motor, i.e. it turns together with the stepping motor, and the friction between the inside housing wall and the inertial disk effects the damping.

The invention is based on the object of improving an engraving element of
25 an electronic engraving machine for engraving printing forms as well as a damping mechanism for an engraving element such that the movement of the engraving stylus of the engraving element is optimally damped in order to achieve a high engraving quality.

This object is achieved by the features of claim 1 with respect to the
30 engraving element and is achieved by the features of claim 25 with respect to the damping mechanism.

3a

Advantageous improvements and developments are recited in the subclaims.

The invention is explained in greater detail below with reference to Figs. 1
5 5 through 9.

Shown are:

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- Fig. 1 the schematic structure of an engraving element having a damping mechanism in a perspective view;
- Fig. 2 an exemplary embodiment of a rotational-symmetrical damping mechanism having a circular or circular sector-shaped damping disk, shown in section;
- 5 Fig. 3 an exemplary embodiment of a non-rotational symmetrical damping mechanism having a circular segment-shaped damping disk, shown in section;
- Fig. 4 an exemplary embodiment of a rotational-symmetrical damping mechanism having two circular or circular sector-shaped damping disks, shown in section;
- 10 Fig. 5 an exemplary embodiment of a non-rotational-symmetrical damping mechanism having two circular segment-shaped damping disks, shown in section;
- 15 Fig. 6 a development of a rotational-symmetrical damping mechanism having an integrated spoke bearing, shown in section;
- Fig. 7 a development of a non-rotational-symmetrical damping mechanism having an integrated spoke bearing, shown in section;
- Fig. 8 a perspective illustration of a rotational-symmetrically fashioned spoke bearing; and
- 20 Fig. 9 a perspective illustration of a non-rotational-symmetrically fashioned spoke bearing.

Fig. 1 shows a perspective illustration of the structure of an engraving element that is fundamentally composed of a drive system - of an electromagnetic drive system in the illustrated example - and of a rotatory system.

25

The electromagnetic drive element is composed of a stationary electromagnet (1) having two u-shaped plate packets (2) lying opposite one another and two air gaps (3) lying between the legs of the plate packets (2). A coil (5) - which is shown from only coil side - is located in the recesses (4) of the plate packets (2) of the electromagnet (1). The coil (5) has an engraving control signal flowing through it.

30

The rotatory system is composed of a shaft (6), of an armature (7) secured to the shaft (6), as well as of a damping mechanism (8) and a spoke bearing (9) for the shaft (6). The armature (7) is movable in the air gaps (3) of the electromagnet (1). One shaft end merges into a resilient torsion bar (10) that is clamped in a stationary bearing (11, 12). The other shaft end (13) carries a lever (14) to which the engraving stylus (15) is attached. The damping mechanism (8) and the spoke bearing (9) are arranged between the armature (7) and the lever (14) with the engraving stylus (15). As a result of the magnetic field generated in the air gaps (2) [sic] of the electromagnet (1), an electrical torque is exerted on the armature (7) of the shaft (6), this electrical torque being opposed by the mechanical torque of the torsion bar (10). The electrical torque turns the shaft (6) around its longitudinal axis with a rotational angle proportional to the respective engraving control signal value, turning this out of a quiescent position, and the torsion bar (10) returns the shaft (6) into the quiescent position. As a result of the rotatory motion of the shaft (6), the engraving stylus (15) implements a stroke directed in the direction onto the generated surface of a printing cylinder (not shown) that defines the penetration depth of the engraving stylus (15) into the printing cylinder. When engraving, the rotatory system executes an oscillation motion dependent on the frequency of the raster signal by a very small rotational angle of, for example, a maximum of $\pm 0.5^\circ$, this corresponding to a maximum stroke of approximately $250 \mu\text{m}$ of the engraving stylus (15).

The drive system for the engraving stylus (15) can also be fashioned as a solid-state actuator element that, for example, can be formed for a piezoelectric or of a magnetostrictive material.

Fig. 2 shows an exemplary embodiment of a rotational-symmetrical damping mechanism (8) having a circular or circular sector-shaped damping disk (17).

Fig. 2a shows a sectional view of the damping mechanism (8) in axial direction of the shaft (6). The damping mechanism (8) is essentially composed of a damping disk (17) that is connected to the shaft (6) and expands perpendicular to the shaft (6) and is further composed of a stationary damping chamber (18). The damping disk (17) is fashioned as at least one damping wing (Fig. 2c) rotational-symmetrically

relative to the shaft (6) either circularly (Fig. 2b) or circular sector-shaped. The stationary damping chamber (18) is fashioned as a rotational-symmetrical hollow cylinder around the shaft (6) having a u-shaped cross-section into whose interior facing toward the shaft (6) the damping disk (17) immerses. When the damping disk (17) is fashioned as at least one damping wing, the damping chamber (18) can be composed of hollow cylinder segments that respectively extend at least over a damping wing (17). The stationary damping chamber (18) is composed of a disk-shaped base plate (20), of a disk-shaped cover plate (21) and of a spacer ring (22) lying between base plate (20) and cover plate (21). The base plate (20) and the cover plate (21) comprise through openings (23, 24) for the shaft (6). Base plate (20), cover plate (21) and spacer ring (22) are arranged such relative to one another and connected to one another with, for example, screws (25) that they form the interior of the damping chamber (18). The spacer ring (22) is dimensioned that a defined damping gap (26) for the acceptance of a damping fluid arises between base plate (20), cover plate (21) and spacer ring (22) on the one hand and the damping surfaces of the damping disk (17) on the other hand.

The diameter of the through opening (24) in the cover plate (21) is selected such that an additional damping gap (26') for the damping fluid is formed between the inside surface that faces toward the shaft (6) and the generated surface of the shaft (6). The damping disk (17) can be provided with through holes (27) proceeding in axial direction of the shaft (6). The through holes (27) form connecting channels to the damping gaps (26) above and below the damping disk (17) and advantageously serve for compensating the damping fluid and as a reservoir for the damping fluid. Over and above this, the through holes (27) reduce axial vibrations of the damping disk (17).

A ferro-fluidic fluid is preferably employed as damping fluid in the damping chamber (18). A ferro-fluidic fluid is a colloidal solution of magnetic particles in an oil that can be magnetized. A ferro-fluidic fluid is commercially obtainable under the trade name Ferrofluidics® of ferro fluidics GmbH.

The degree of attenuation that can be achieved with a damping fluid is advantageously independent of the respectively preceding deformation, so that no

"memory" effect arises that would lead to disturbing engraving errors. Over and above this, the degree of damping that can be achieved with a damping fluid can be approximately calculated. A high temperature stability and long-term stability of the degree of damping is also achieved with a damping fluid, since the heat arising as a result of high engraving frequencies can be eliminated well via the damping fluid.

The described exemplary embodiment employs a ferrofluidic damping fluid that is held in the damping gap (26) by a magnetic field generated with a magnet, as a result whereof complicated seals can be eliminated. In the exemplary embodiment, an annular retaining magnet (28) for the ferro-fluid is located in an annular channel (29) in the base plate (20) of the damping chamber (18). In order to prevent dust from entering into the damping chamber (18), a seal ring (30) embracing the shaft (6) can be provided, this being located in a recess (31) of the base plate (20).

Fig. 2b shows a section through the damping mechanism (8) in a plane proceeding perpendicular to the axial direction of the shaft (6). The sectional view shows the circularly fashioned damping disk (17).

Fig. 2c again shows a section through the damping mechanism (8) in a plane proceeding perpendicular to the axial direction of the shaft (6). The sectional view shows the fashioning of the circular sector-shaped damping disk (17) as two damping wings.

Fig. 3 shows an exemplary embodiment of a non-rotational-symmetrical damping mechanism (8) having a circular segment-shaped damping disk (17).

Fig. 3a again shows a section through the damping mechanism (8) in axial direction of the shaft (6), whereby the damping disk (17) and the damping chamber (18) are fashioned as circular or, respectively, hollow-cylindrical segments that are not rotationally symmetrical with respect to the axis of the shaft (6). This embodiment can be advantageously employed when an optimally slight distance of the shaft (6) of the engraving element from the generated surface of a printing cylinder is desired. The damping disk (17) is fashioned as circular segment, whereby the edge of the damping disk (17) forming the chord lies as close as possible to the shaft (6). The damping chamber (18) is fashioned as hollow cylinder segment corresponding to the shape of the damping disk (17) fashioned as circular segment.

The fundamental structure of the damping chamber (18) is basically identical to the structure of the damping chamber (18) shown in Fig. 2a.

Fig. 3b shows a section through the damping mechanism (8) in a plane proceeding perpendicular to the axial direction of the shaft (6). The sectional view shows the
5 fashioning of the damping disk (17) as circular segment.

Fig. 4 shows an exemplary embodiment of a rotational-symmetrical damping mechanism (8) having two circular or circular sector-shaped damping disks (17, 17') in a section in axial direction of the shaft (6).

The damping mechanism (8) is basically constructed like the damping
10 mechanism (8) according to Fig. 2a). It differs from the damping mechanism (8) shown in Fig. 2a in that two damping disks (17, 17') arranged parallel to one another and spaced from one another in axial direction of the shaft (6) are connected as double disk to the shaft (6), and in that the damping chamber (18) is divided by an intermediate plate (32) in two sub-chambers (33, 33') for the two damping disks (17,
15 17'). The intermediate plate (32) is thereby dimensioned such that the two sub-chambers (33, 33') are connected to one another by an additional damping gap (26'). The damping disks (17, 17') are shaped as shown in Fig. 2a or Fig. 2c).

Fig. 5 shows an exemplary embodiment of a non-rotational-symmetrical damping mechanism (8) having two circular segment-shaped damping disks (17, 17')
20 in a sectional view in axial direction of the shaft (6). The damping mechanism (8) is fundamentally constructed as described in Fig. 4. The damping disks (17, 17') are shaped as shown in Fig. 3b.

The damping disk (17) is made, for example, of aluminum or steel. Base plate (20), cover plate (21), spacer ring (22) and intermediate plate (32) are preferably
25 composed of non-magnetic material.

The two damping disks (17, 17') can be supplemented by further damping disks. The employment of more than one damping disk has the advantage that a higher degree of damping is achieved due to the increased damping area that interacts with the damping fluid. Given an identical damping area, the diameter of the
30 individual damping disks can be reduced given employment of a plurality of damping disks. This preferably leads to a lower mass moment of inertia and to lower

circumferential speeds at the edges of the damping disks. This reduces the risk that the damping fluid will modify and deteriorate the damping property.

Fig. 6 shows a development wherein the rotational-symmetrical damping mechanism (8) is structurally combined with the rotational-symmetrically fashioned spoke bearing (9).

Fig. 6a shows a section through the damping mechanism (8) in axial direction of the shaft (6), this agreeing with the sectional view of the damping mechanism (8) shown in Fig. 2a except for the spoke bearing (9). The rotational-symmetrical spoke bearing (9) is composed of an inside ring (35) embracing the shaft (6) and connected thereto, of a stationary outer ring (36) surrounding the shaft (6) and spaced from the inner ring (35), and of a plurality of leaf springs (37) proceeding radially at identical or irregular angular spacings. The broadsides are directed in axial direction of the shaft (6), so that the inner ring (35) is torsionally seated relative to the stationary outer ring (36), namely around the longitudinal axis of the shaft (6). The ends of the leaf springs (37) are respectively clamped in the two rings (35, 36). Outer ring (36) and cover plate (21) of the damping chamber (18) are preferably fabricated as one component part.

Fig. 6b shows a section through the rotational-symmetrical spoke bearing (9) in a plane proceeding perpendicular to the axial direction of the shaft (6).

Fig. 7 shows a development wherein the non-rotational-symmetrical damping mechanism (8) is structurally united with the non-rotationally-symmetrically fashioned spoke bearing (9).

Fig. 7a shows a section through the non-rotational-symmetrical damping mechanism (8) in axial direction of the shaft (6), this coinciding with the section through the damping mechanism (8) shown in Fig. 3a except for the structurally integrated spoke bearing (9). The non-rotational-symmetrical spoke bearing (9) is composed of an inner ring (35) that surrounds the shaft (36) and is connected thereto, of a stationary outer ring segment (36') that surrounds the shaft (6) and is spaced from the inner ring (35'), and of a plurality of radially proceeding leaf springs (37') whose broad sides are likewise directed in axial direction of the shaft (6) and whose ends are respectively secured in the inner ring (35') and in the outer ring segment (36'). Outer

ring segment (36') and circular segment-shaped cover plate (21) of the damping chamber (18) are again a shared component part.

Fig. 7b shows a section through the non-rotational-symmetrical spoke bearing (9) in a plane proceeding perpendicular to the axial direction of the shaft (6).

5 Fig. 8 shows a perspective view of a rotational-symmetrically fashioned spoke bearing (9).

Fig. 9 shows a perspective view of a non-rotational-symmetrically fashioned spoke bearing (9).

Patented 1960

PATENT CLAIMS

1. Engraving element of an electronic engraving machine for engraving printing forms, composed of:

- a shaft (6) oscillating around the longitudinal axis with small rotational angles;
 - a drive system (1, 7) for the shaft (6);
 - a lever (14) attached to an end of the shaft (6) with an engraving stylus (15) for engraving the printing form;
 - a restoring element (10) for the shaft (6);
 - a bearing (9) for the shaft (6); and
 - a damping mechanism (8) for the shaft (6) having a damping element secured to the shaft (6) as well as a stationary damping chamber filled with a damping medium,
- characterized in that
- the damping medium is a ferro-fluidic fluid.

2. Engraving element according to claim 1, characterized in that the damping mechanism (8) is not fashioned rotationally symmetrical relative to the axial direction of the shaft (6).

3. Engraving element according to claim 1, characterized in that the damping element (17) is provided with through holes (27) proceeding in axial direction of the shaft (6).

4. Engraving element according to claim 1, characterized in that the bearing (9) for the shaft (6) is fashioned as spoke bearing.

5. Engraving element according claim 4, characterized in that the spoke bearing (9) is composed of the following components:

- an inner ring (35, 35') surrounding the shaft (6) and connected to the shaft (6);

- a stationary outer ring (36) or, respectively, outer ring segment (36') surrounding the shaft (6) at least in regions and spaced from the inner ring (35, 35'); and
- a plurality of leaf springs (37) proceeding radially relative to the shaft (6) whose ends are respectively connected to the inner rings (35, 35') and to the outer ring (36) or, respectively, outer ring segment (36').

6. Engraving element according to claim 4, characterized in that the damping mechanism (18) and the spoke bearing (9) are structurally united with one another.

7. Engraving element according to claim 1, characterized in that the drive system (1, 7) for the shaft (6) is fashioned as piezoelectric or magnetostrictive drive element.

8. Damping mechanism for an engraving element for engraving printing forms, composed of

- a damping element (17) that is secured to a shaft (6) of the engraving element oscillating around the longitudinal axis with small rotational angles, and
- a stationary damping chamber filled with a damping medium, characterized in that
- the damping medium is a ferro-fluidic fluid.

9. Damping mechanism according to claim 8, characterized in that it is not fashioned rotational-symmetrically to the axial direction of the shaft (6).

10. Damping mechanism according to claim 8, characterized in that the damping element (17) is provided with through holes (27) proceeding in axial direction of the shaft (6).

ABSTRACT

The invention is directed to an engraving element of an electronic engraving machine for engraving printing forms. The engraving element is composed of a shaft (6) oscillating around the longitudinal axis with small rotational angles, of a drive system (1, 7) for the shaft (6), of a lever (14) attached to one end of the shaft (6) with an engraving stylus (15) for engraving the printing form, of a restoring element (11) for the shaft (6), a bearing (8) for the shaft (6) and a damping mechanism (8) for the shaft (6) having a damping element secured to the shaft (6) and a stationary damping chamber. The damping element comprises at least one damping disk that is fashioned circularly at least in regions and extends perpendicular to the shaft (6). The damping chamber is fashioned at least as a hollow-cylindrical segment around the shaft (6) into which the damping disk projects and extends at least over the circular region of the damping disk. The damping chamber is filled with a ferro-fluidic fluid as damping agent.

Figure 1

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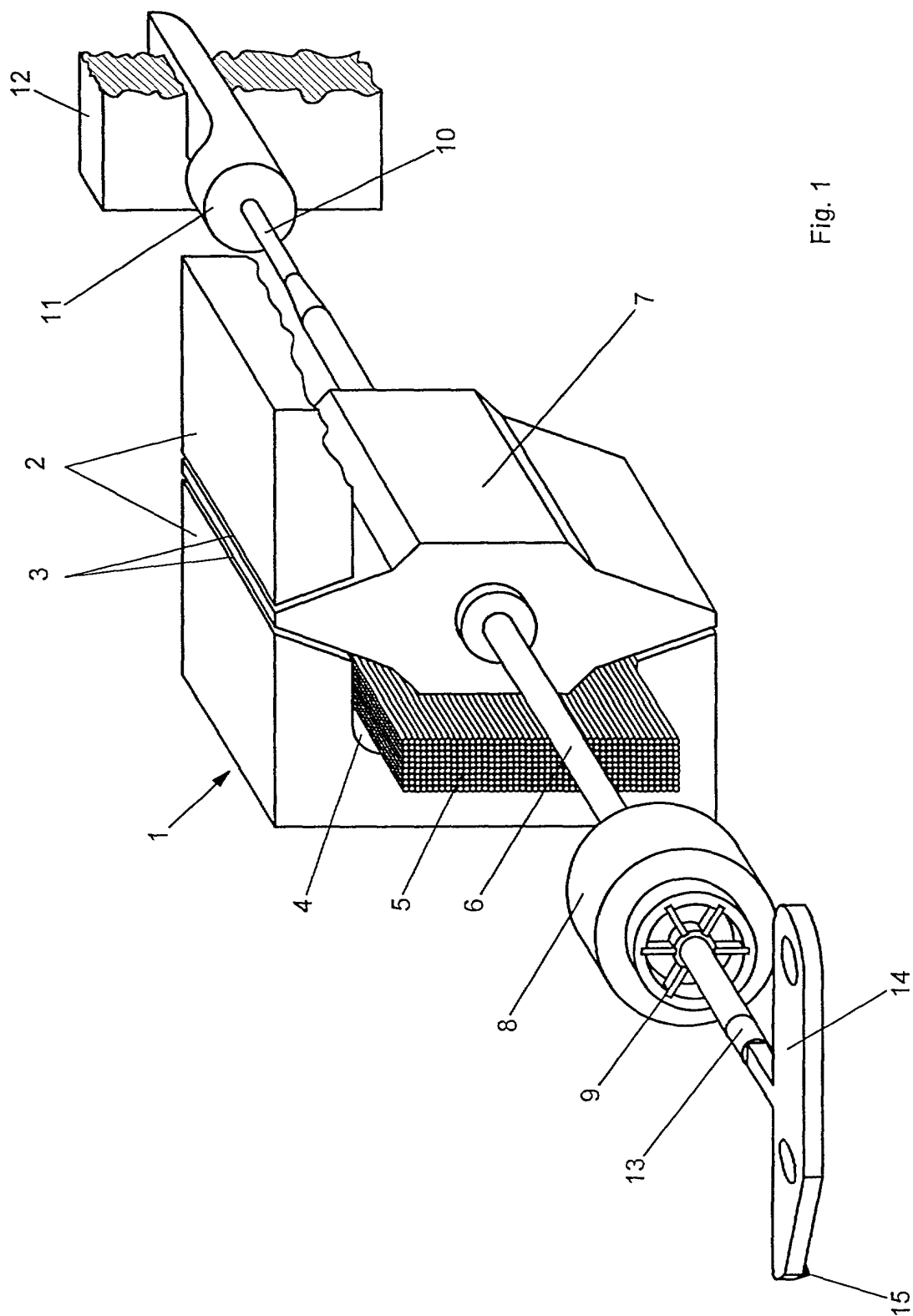


FIG. 1

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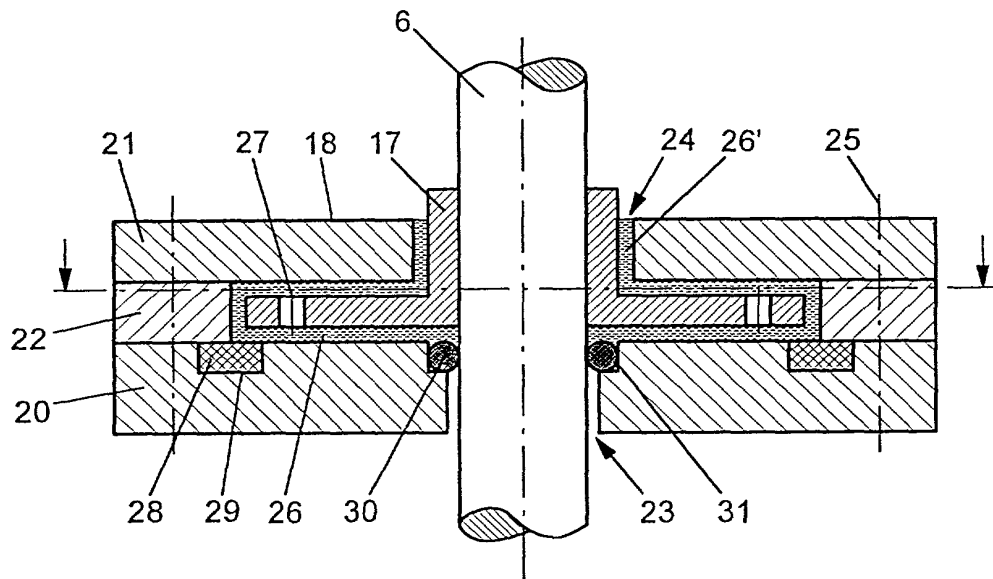


Fig. 2a

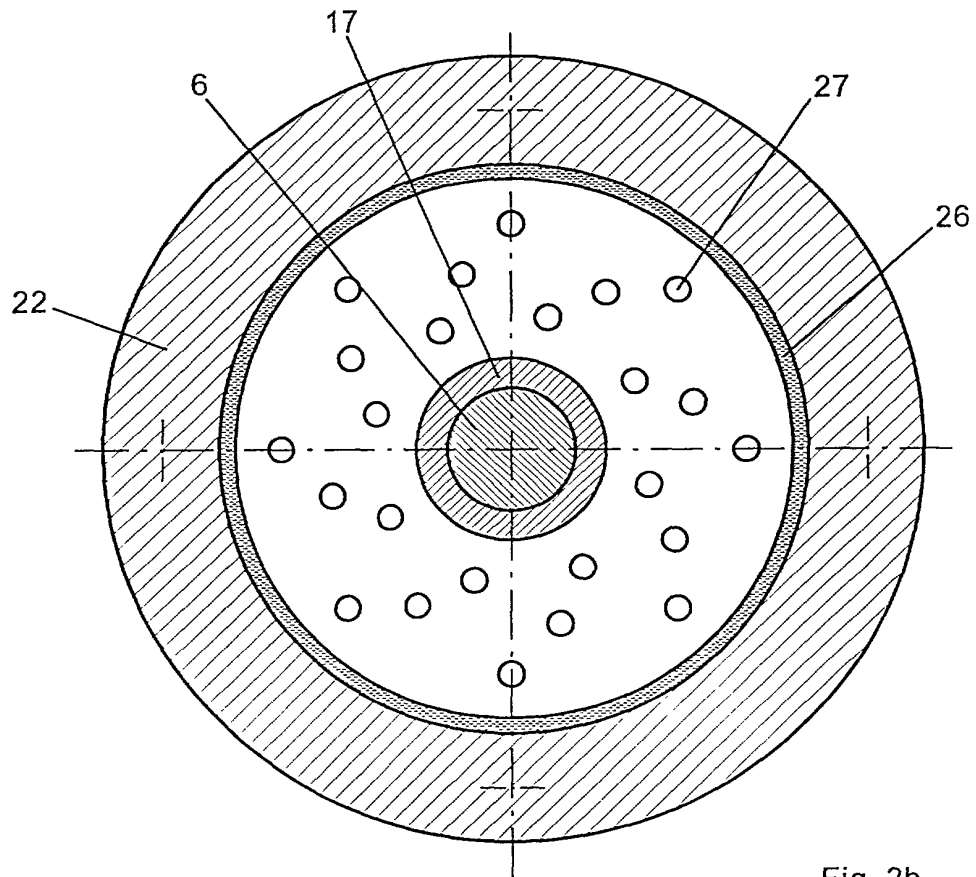


Fig. 2b

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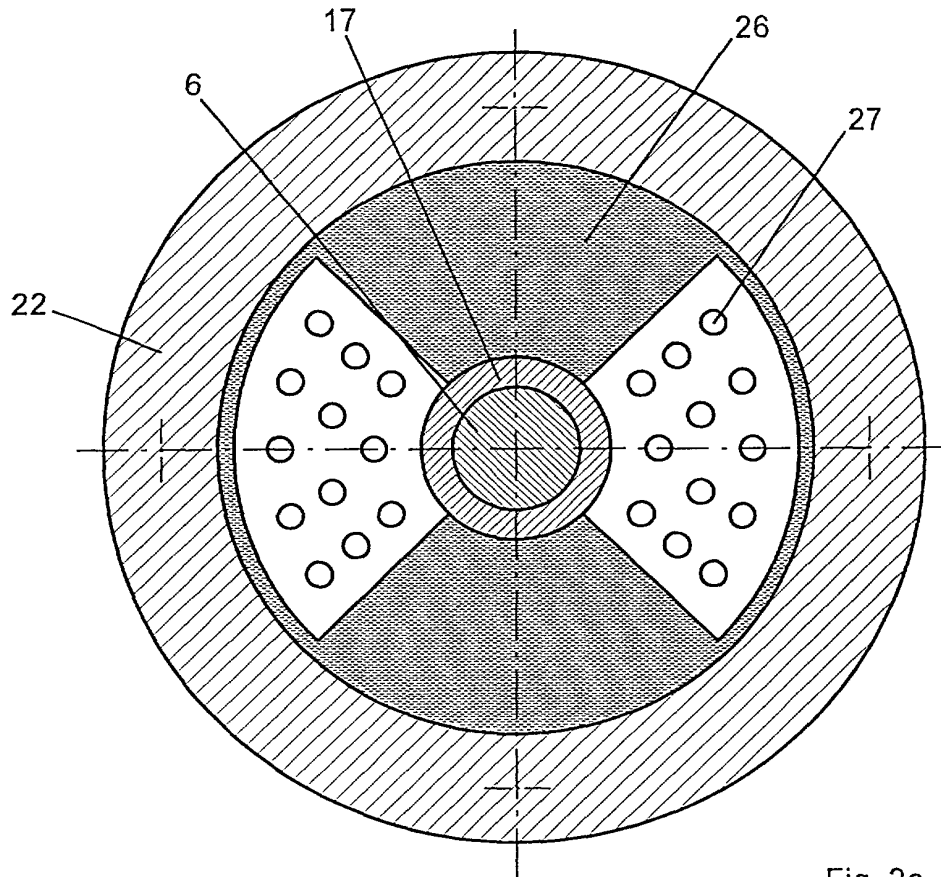


Fig. 2c

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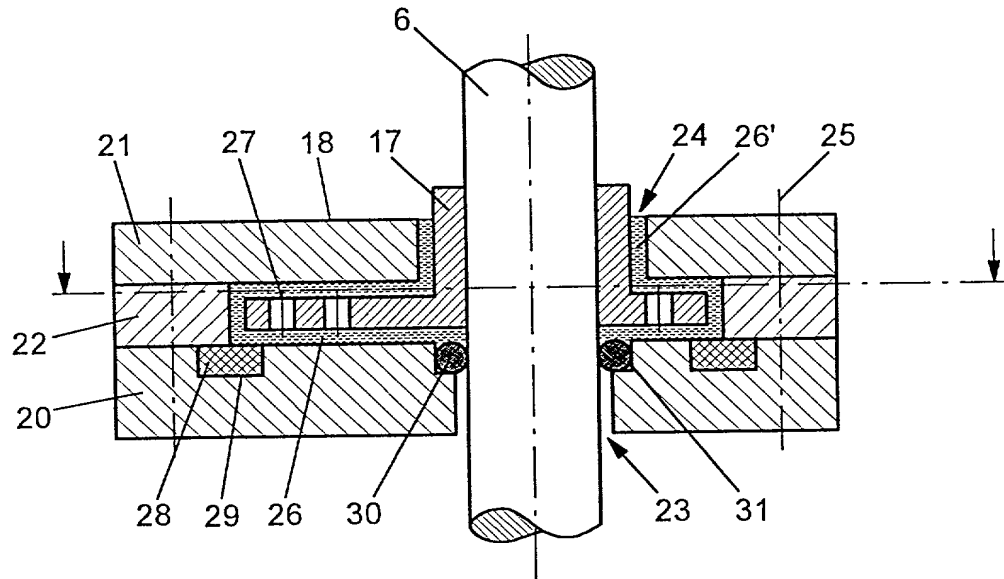


Fig. 3a

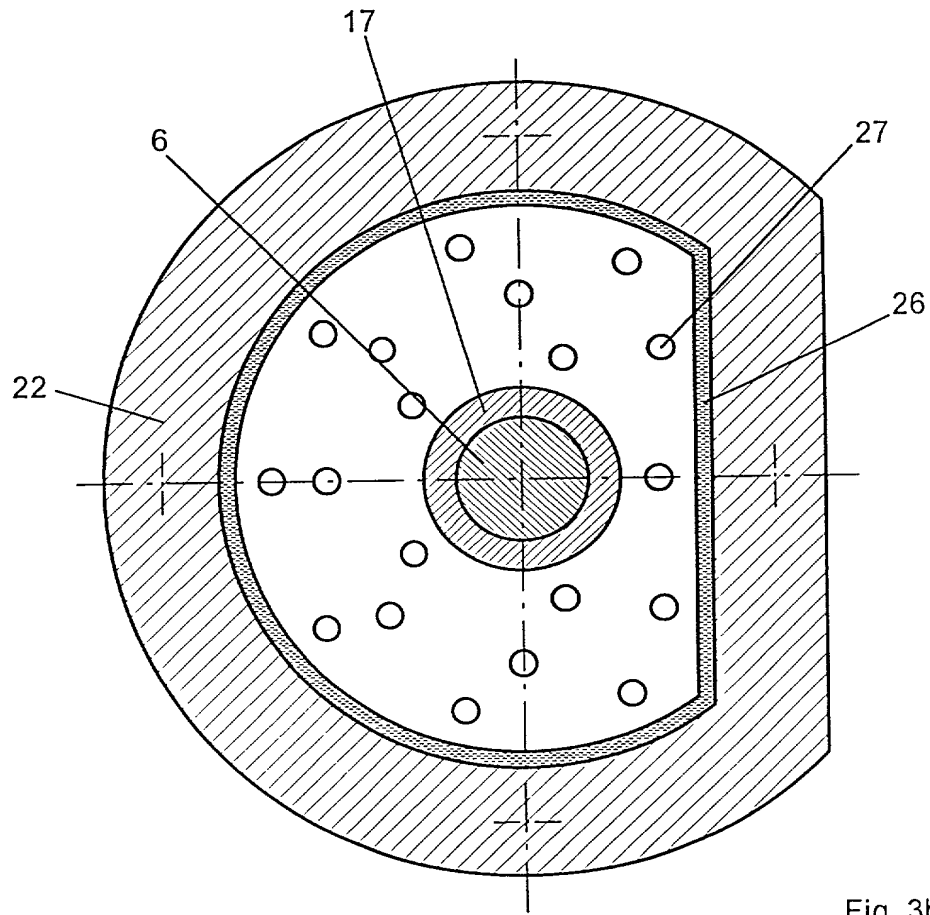


Fig. 3b

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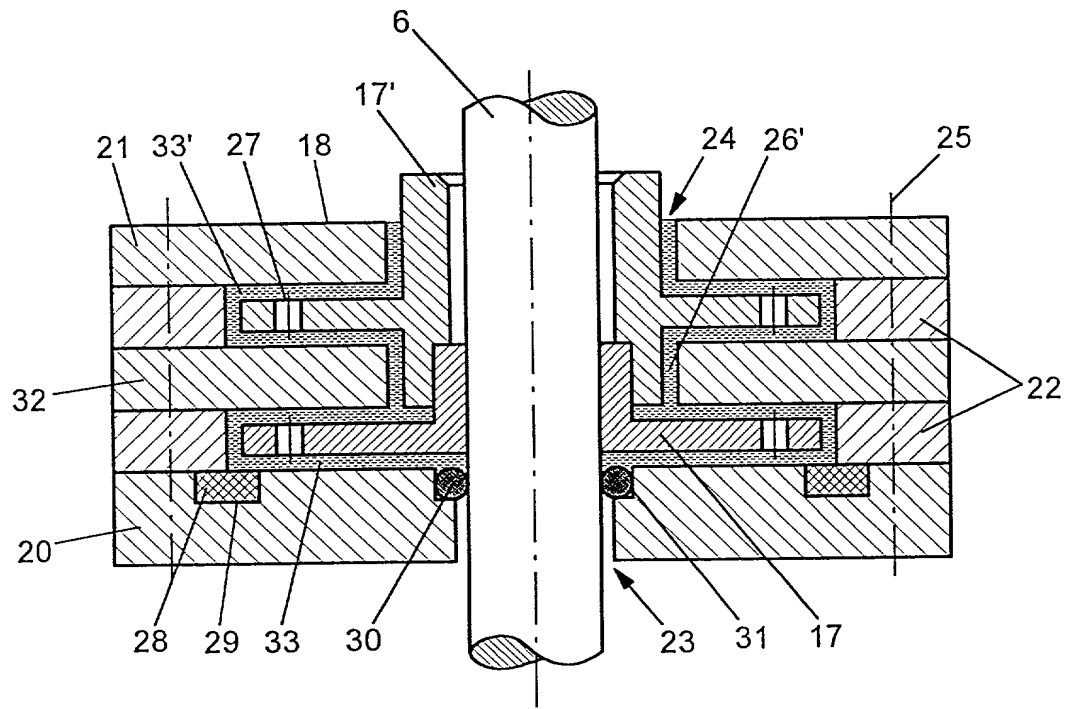


Fig. 4

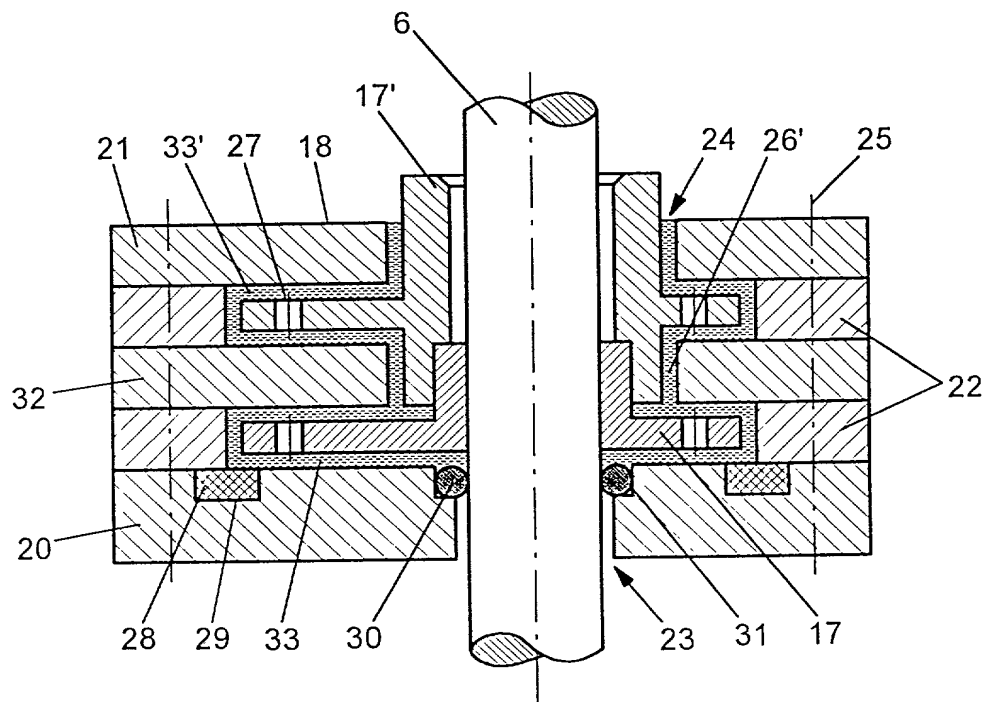


Fig. 5

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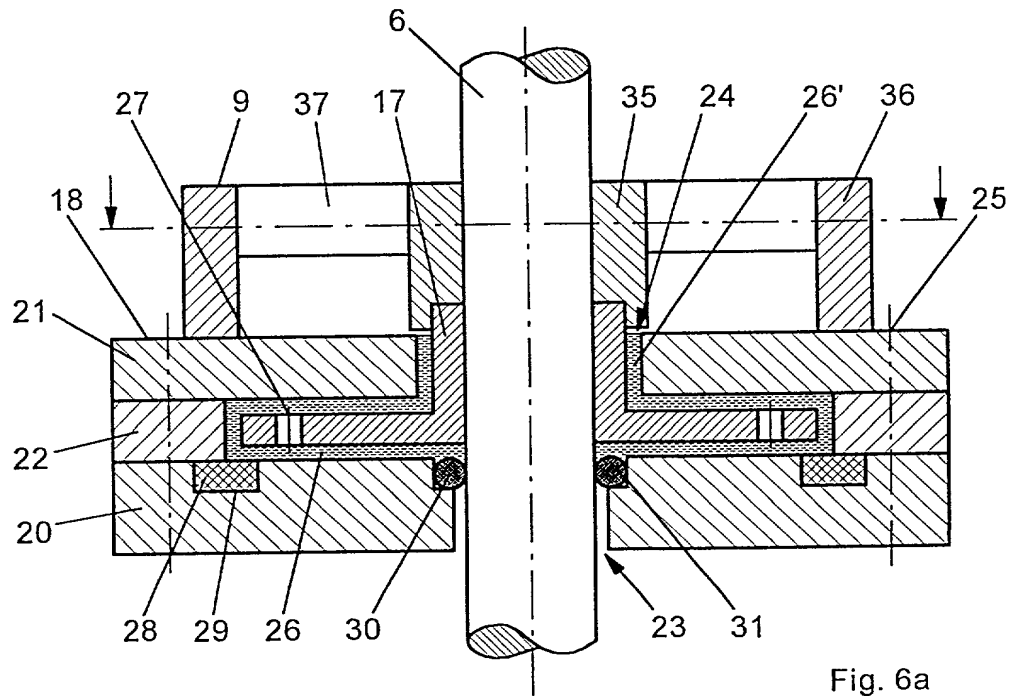


Fig. 6a

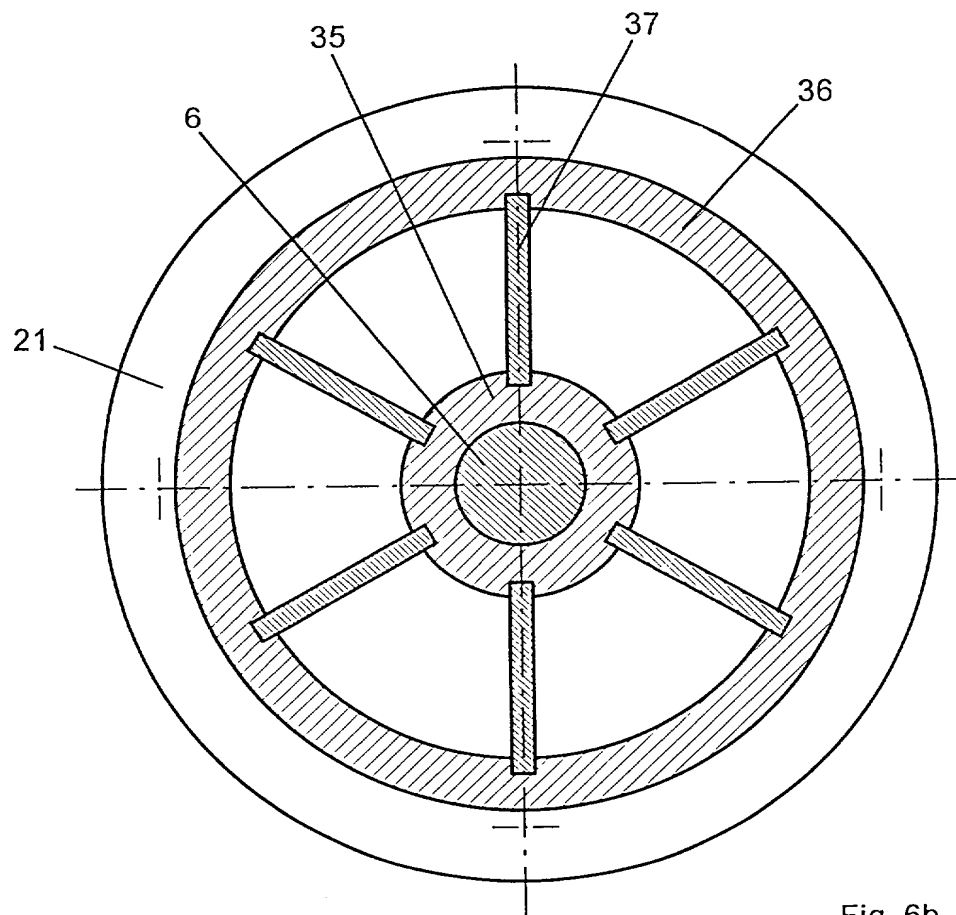


Fig. 6b

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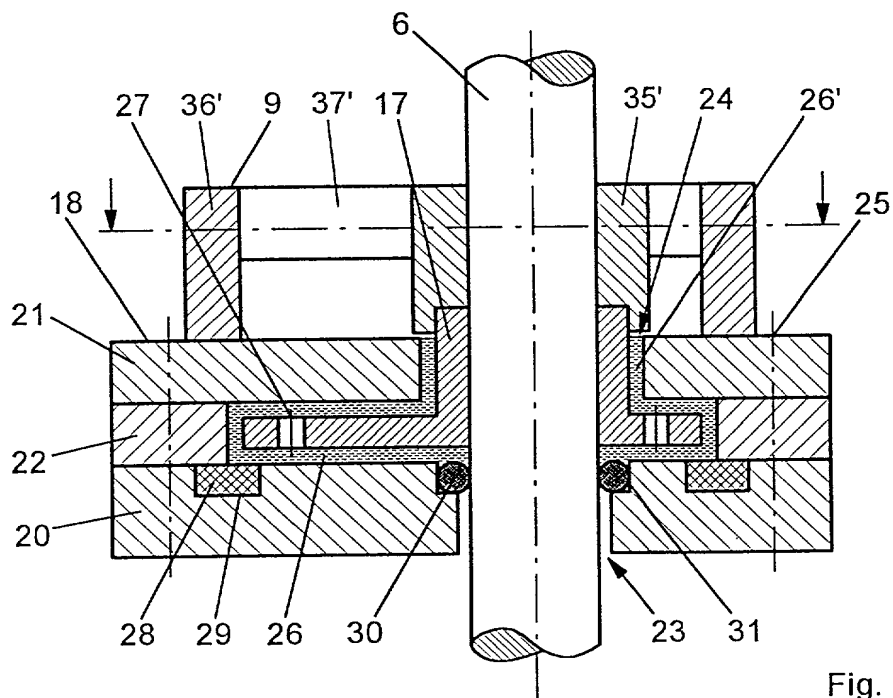


Fig. 7a

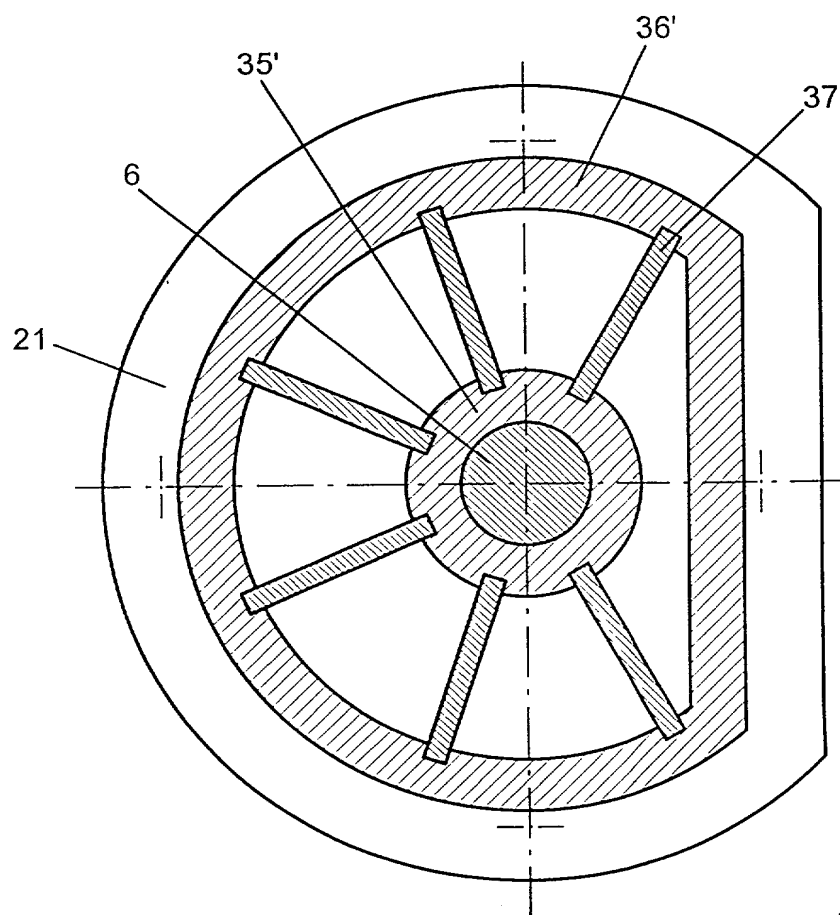


Fig. 7b

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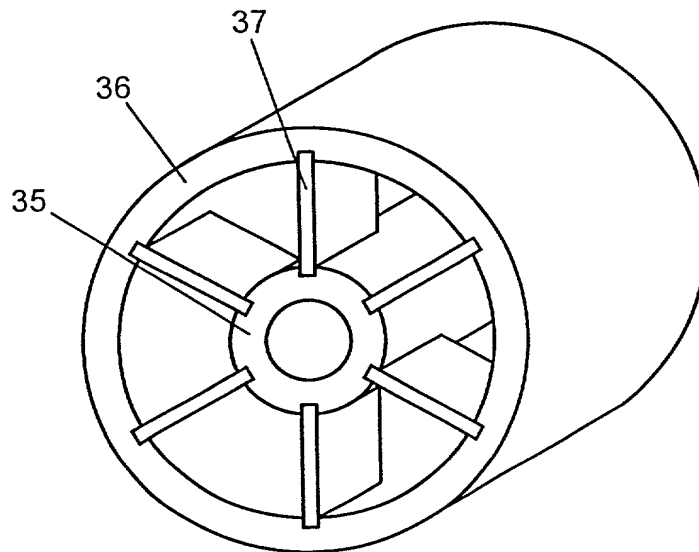


Fig. 8

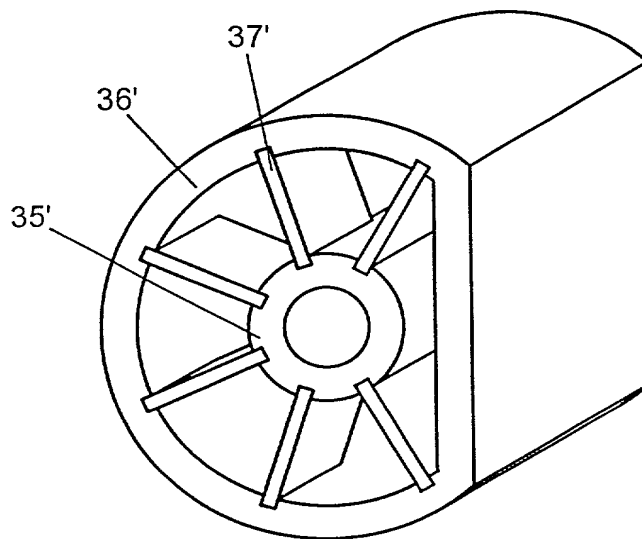


Fig. 9

FIG. 8

Combined Declaration For Patent Application and Power of Attorney

ATTORNEY'S DOCKET NO.

(Continued)

P00,1899

(Includes Reference to PCT International Applications) PCT/DE99/01700

I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) or PCT international application(s) designating the United States of America that is/are listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in that/those prior application(s) in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, §1.56(a) which occurred between the filing date of the prior application(s) and the national or PCT international filing date of this application:

PRIOR U.S. APPLICATIONS OR PCT INTERNATIONAL APPLICATIONS DESIGNATING THE U.S. FOR BENEFIT UNDER 35 U.S.C. 120:

U.S. APPLICATIONS			STATUS (Check one)		
U S APPLICATION NUMBER	U.S. FILING DATE		PATENTED	PENDING	ABANDONED
PCT APPLICATIONS DESIGNATING THE U.S.					
PCT APPLICATION NO	PCT FILING DATE	U.S. SERIAL NUMBERS ASSIGNED (if any)			

POWER OF ATTORNEY: And I hereby appoint Messrs. John D. Simpson (Registration No. 19,842), Steven H. Noll (28,982), Brett A. Valiquet (27,841), James D. Hobart (24,149), Melvin A. Robinson (31,870), and Mark Bergner (45,877), all members of the firm of Schiff, Hardin & Waite

Send Correspondence to:

SCHIFF HARDIN & WAITE
Patent Department
6600 Sears Tower, Chicago, Illinois 60606

Direct Telephone Calls to:

312/258-5500
Ext. 5786

201	FULL NAME OF INVENTOR	FAMILY NAME <u>Carstens</u>	FIRST GIVEN NAME <u>Dieter</u>	SECOND GIVEN NAME
	RESIDENCE & CITIZENSHIP	CITY <u>Kiel</u> <u>DEX</u>	STATE OR FOREIGN COUNTRY <u>GERMANY</u>	COUNTRY OF CITIZENSHIP <u>GERMANY</u>
	POST OFFICE ADDRESS	POST OFFICE ADDRESS <u>Gabelsberger Str. 15</u>	CITY <u>24148 Kiel</u>	STATE & ZIP CODE/COUNTRY <u>GERMANY</u>
202	FULL NAME OF INVENTOR	FAMILY NAME	FIRST GIVEN NAME	SECOND GIVEN NAME
	RESIDENCE & CITIZENSHIP	CITY	STATE OR FOREIGN COUNTRY	COUNTRY OF CITIZENSHIP
	POST OFFICE ADDRESS	POST OFFICE ADDRESS	CITY	STATE & ZIP CODE/COUNTRY
203	FULL NAME OF INVENTOR	FAMILY NAME	FIRST GIVEN NAME	SECOND GIVEN NAME
	RESIDENCE & CITIZENSHIP	CITY	STATE OR FOREIGN COUNTRY	COUNTRY OF CITIZENSHIP
	POST OFFICE ADDRESS	POST OFFICE ADDRESS	CITY	STATE & ZIP CODE/COUNTRY

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application of any patent issuing thereon.

SIGNATURE OF INVENTOR 201	SIGNATURE OF INVENTOR 202	SIGNATURE OF INVENTOR 203
DATE <u>10.01.2001</u>	DATE	DATE

COMBINED DECLARATION FOR PATENT APPLICATION AND POWER OF ATTORNEY(Includes Reference to PCT International Applications) **PCT/DE99/01700**ATTORNEY'S
DOCKET NUMBER
P00,1899

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name,
I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor
(if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the
invention entitled:

"ENGRAVING ELEMENT"

the specification of which (check only one item below):

- ☐ is attached hereto.
- ☐ was filed as United States application
Serial No. _____
on _____,
and was amended
on _____ (if applicable).
- ☒ was filed as PCT international application
Number **PCT/DE99/01700**
on **10 June 1999**,
and was amended under PCT Article 19
on _____ (if applicable).

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the
claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to the examination of this application in accordance
with Title 37, Code of Federal Regulations, §1.56(a).

I hereby claim foreign priority benefits under Title 35, United States Code, §119 of any foreign application(s) for patent
or inventor's certificate or of any PCT international application(s) designating at least one country other than the
United States of America listed below and have also identified below any foreign application(s) for patent or inventor's
certificate or any PCT international application(s) designating at least one country other than the United States of
America filed by me on the same subject matter having a filing date before that of the application(s) of which priority is
claimed:

PRIOR FOREIGN/PCT APPLICATION(S) AND ANY PRIORITY CLAIMS UNDER 35 U.S.C. 119:

COUNTRY (if PCT indicate "PCT")	APPLICATION NUMBER	DATE OF FILING (day, month, year)	PRIORITY CLAIMED UNDER 35 USC 119
GERMANY	198 30 471.4	08 July 1998	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO
			<input type="checkbox"/> YES <input type="checkbox"/> NO
			<input type="checkbox"/> YES <input type="checkbox"/> NO
			<input type="checkbox"/> YES <input type="checkbox"/> NO
			<input type="checkbox"/> YES <input type="checkbox"/> NO